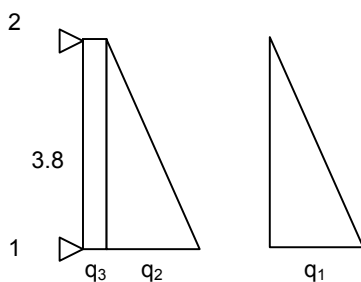


APPENDIX 20

STRUCTURAL CALCULATION OF CLEAN WATER RESERVOIR

- Belasting op dek max 0.5 m grond
- Veranderlijk 4.0 kN/m^2 (NEN 7602)
- Max waterstand NAP +4.60
- Aangehouden tot o.k. dek NAP +4.80
- HGS onder bodem kelder

Kelderwand



Inwendig

$$q_1 \text{ water} = 3.55 \times 10.0 = 35.5 \text{ kN/m'}$$

$$q_d = 42.6 \text{ kN/m'}$$

Uitwendig

$$q_2 \text{ grond} = 3.55 \times 20.0 \times 0.5 = 35.5 \text{ kN/m'}$$

$$q_3 \text{ b.b} = (0.5 \times 20.0 + 4.0) \times 0.5 = 7 \text{ kN/m'}$$

1

$$q_{2d} = 1.35 \times 35.5 = 47.925 \text{ kN/m'}$$

$$q_{3d} = 1.35 \times 0.5 \times 20.0 \times 0.5 = 6.75 \text{ kN/m'}$$

resp

$$q_{2d} = 1.2 \times 35.5 = 42.6 \text{ kN/m'}$$

$$q_{3d} = (1.2 \times 0.5 \times 20.0 + 1.5 \times 4.0) \times 0.5 = 9 \text{ kN/m'}$$

Mv bij vrij opgelegd

t.g.v. q_1

$$M_d = 1/27 \times 3^{1/2} \times 42.6 \times 3.8^2 = 39.46 \text{ kNm}$$

t.g.v. q_2, q_3

$$M_d = 1/27 \times 3^{1/2} \times 47.925 \times 3.8^2 + 1/8 \times 6.75 \times 3.8^2 = 56.58 \text{ kNm}$$

t.q.v. resp

$$M_d = 1/27 \times 3^{1/2} \times 42.6 \times 3.8^2 + 1/8 \times 9 \times 3.8^2 = 55.71 \text{ kNm}$$

1

$$V_{1d} = 2/3 \times 1/2 \times 3.8 \times 47.925 + 0.5 \times 3.8 \times 6.75 = 73.53 \text{ kN/m'}$$

$$V_{2d} = 1/3 \times 1/2 \times 3.8 \times 47.925 + 0.5 \times 3.8 \times 6.75 = 43.18 \text{ kN/m'}$$

resp

$$V_{1d} = 2/3 \times 1/2 \times 3.8 \times 42.6 + 0.5 \times 3.8 \times 9 = 71.06 \text{ kN/m'}$$

$$V_{2d} = 1/3 \times 1/2 \times 3.8 \times 42.6 + 0.5 \times 3.8 \times 9 = 44.08 \text{ kN/m'}$$

$$h = 250 \text{ mm} \quad d = 200 \text{ mm}$$

$$\tau_d = 73.53/200 = 0.37 \text{ N/mm}^2 < \tau_1 (= 0.56 \text{ N/mm}^2)$$

$$\text{Max } M_d = 56.58 \text{ kNm/m'}$$

$$b \times d = 1.0 \times 0.2 \quad M_d/bd^2 = 1414.5$$

$$\omega_0 = 0.337$$

$$A = 674 \text{ mm}^2 \rightarrow \phi 12-165$$

Bij volledige inklemming in bodem en dek

t.g.v. q_1

$$M_d = 1/20 \times 42.6 \times 3.8^2 = 30.76 \text{ kNm}$$

t.g.v. q_2, q_3

$$M_d = 1/20 \times 47.925 \times 3.8^2 + 1/12 \times 6.75 \times 3.8^2 = 42.72 \text{ kNm}$$

t.q.v. resp

$$M_d = 1/20 \times 42.6 \times 3.8^2 + 1/12 \times 9 \times 3.8^2 = 41.59 \text{ kNm}$$

$$\text{Max } M_d = 42.72 \text{ kNm/m'}$$

$$b \times d = 1.0 \times 0.2 \quad M_d/bd^2 = 1068$$

$$\omega_0 = 0.252$$

$$A = 505 \text{ mm}^2 \rightarrow \phi 12-220$$

Ivm. Scheurwijdte beperking in milieuklasse 5

$$\text{Bij } \phi 12 \quad \omega_0 = 0.33 \rightarrow \phi 12-125$$

Kelder dek $h = 250 \text{ mm}$

Belasting permanent

▪ Eigen gewicht	0.25×25	$= 6.25 \text{ KN/m}^2$
▪ Isolatie + dakbed		$= 0.75 \text{ KN/m}^2$
▪ Grond	0.5×20	$= 10 \text{ KN/m}^2$
		$= 17 \text{ KN/m}^2$
		$= 4 \text{ KN/m}^2$

Veranderlijk

BC 1 $P_d = 1.2 \times 17.0 + 1.5 \times 4.0 = 26.4 \text{ KN/m}^2$

Kolom afstand 3.35×3.35

Kolom afmeting $\phi 300$

$F_d = 3.35 \times 3.35 \times 26.4 = 296.3 \text{ KN}$

Belasting op ponscirkel met diameter $D = 300 + 2 \times 200 = 700 \text{ mm}$

$Q = \frac{1}{4} \pi \times 0.7^2 \times 26.4 = 10.2 \text{ KN}$

$\tau_d = (296.274 - 10.16) / \{\pi \times 0.2 (200+300)\} = 0.91 \text{ N/mm}^2$

$V_{1d} = 1/3 \times \frac{1}{2} \times 3.8 \times 35.5 \times 1.2 = 27 \text{ KN/m}$

Wapening $\rightarrow \phi 12-150 = 754 \text{ mm}^2/\text{m}$ $\sigma_s = 27000/754 = 35.8 \text{ N/mm}^2$

$\tau_1 = 0.8 f_b - \sigma_s / 4 f_s = 1.12 - 35.8 / (4 \times 435) = 1.1 \text{ N/mm}^2 > 0.91 \text{ N/mm}^2 (\tau_d)$

Wapening kelderdek

Maximale momenten NEN 6720

Middenveld (tabel 19) $M = 0.132 \times 26.4 \times 3.35^2 = 39.11 \text{ KNm}$

Randveld (tabel 23) $M = 0.178 \times 26.4 \times 3.35^2 = 52.74 \text{ KNm}$

Hoekveld (tabel 25) $M = 0.19 \times 26.4 \times 3.35^2 = 56.29 \text{ KNm}$

$\rightarrow \text{Max} : M = 56.29 \text{ KNm}$

$M_d/bd^2 = 1407$ $\omega_0 = 0.335$

$A = \omega_0 \times b \times d = 670 \text{ mm}^2$ $\text{min} = \phi 12-150 = 754 \text{ mm}^2$

Ronde kolom $N'd/Ab = 296.274 / (1/4 \times \pi \times 0.3^2) = 4191.42 \text{ KN/m}^2 = 4.19 \text{ N/mm}^2$

$e_t = (e_o + e_c) \xi$

$\psi = 1.31, \rho = 1, l_c = 3550, e_o = 0$

$e_c = 3 [1.5h + e_o (4\psi - 3)] \times (\rho l_c / 100h)^2$
 $= 3 \times 450 \times 0.014 = 18.9$

$\xi = 0.5 (1 + e_1 / e_o) = 0.5$

$e_t = (e_o + e_c) \xi$
 $= 18.9 \times 0.5 = 9.45$

$$\rightarrow e_t = 0.1 \times 300 = 30 \text{ mm}$$

$$B35 \rightarrow f_b = 21, \beta = 1.4$$

$$N'd / (f_b \times A_b) = 4.19 / 21 = 0.2$$

$$N'd \times e_t / (f_b \times A_b \times h) = 0.2 \times 30 / 300 = 0.02$$

$$\rightarrow r = 0 \quad \omega_0 = 0$$

$$A_{min} = 0.3 \times A_b = 212 \text{ mm}^2 \rightarrow 5\phi 12 = (565 \text{ mm}^2)$$

Kelder bodem als dek $\phi 12-150$